said period, d, is established by selecting any two positive integers s and p, such that s > p, and any arbitrary internal angle of incidence, α , calculating the internal angle of diffraction. β , with the following equation:

$$\beta = \text{either } a\cos\left(\frac{2p-1}{2s-1}\right) - \alpha \text{ or } 180 - a\cos\left(\frac{2p-1}{2s-1}\right) - \alpha$$

and using the following equation:

$$d = \frac{\lambda}{n(\sin\alpha + \sin\beta)} ,$$

where λ is the nominal free-space wavelength for which said enhanced volume phase grating is designed,

$$[\alpha + \beta = 2\theta \text{ and}]$$

[
$$2\theta$$
 = either $a\cos\left(\frac{2p-1}{2s-1}\right)$ degrees or $180-a\cos\left(\frac{2p-1}{2s-1}\right)$ degrees,]

[where s and p are integers and s > p > 0,]

and said peak modulation, Δn , of said bulk refractive index is obtained from the following equation:

$$\Delta n = \frac{\lambda}{T} \left(\frac{2s-1}{2} \right) \sqrt{(\cos \alpha)(\cos \alpha - \frac{\lambda}{nd} \tan(\frac{\beta - \alpha}{2}))}.$$

$$[\Delta n = \frac{\lambda}{T}(\frac{2s-1}{2})\sqrt{C_R C_S},]$$

[where
$$C_R = \cos \alpha$$
 and $C_S = \cos \alpha - \frac{\lambda}{nd} \tan(\frac{\beta - \alpha}{2})$;]

values of said bulk refractive index, n, and said peak modulation, Δn , being established using well known exposure and processing procedures for said volume phase medium;

whereby the S-polarization diffraction efficiency and the P-polarization diffraction efficiency of said enhanced volume phase grating, when illuminated by an incident beam of said nominal free-space wavelength, λ , at [an] said internal angle of incidence, α , are simultaneously maximized at a common value of the product ΔnT , thereby simultaneously minimizing insertion loss and PDL in a highly dispersive volume phase grating.

- 10. The enhanced volume phase grating of claim 9 wherein said volume phase medium is dichromated gelatin.
- 11. The enhanced volume phase grating of claim 9 wherein said index modulation, Δn , of said volume phase medium is greater than 0.1, and preferably on the order of 0.2, thereby decreasing Bragg angle sensitivity.
- 12. The enhanced volume phase grating of claim 9 wherein said rigid support means is a transparent medium[, such as glass or fused silica,] and said transparent cover means is a similar or identical transparent medium.
- 13. The enhanced volume phase grating of claim 12 further including a reflective means to reflect the diffracted beam back toward and into said enhanced volume phase grating.
- 14. The enhanced volume phase grating of claim 12 wherein the external surfaces of said transparent medium and said transparent cover means are coated with an anti-reflection coating such that the overall loss for the S-polarized light and the overall loss for the P-polarized light are minimized and substantially equal at said nominal free-space wavelength.
- 15. The enhanced volume phase grating of claim 12 wherein the external surfaces of said transparent medium and said transparent cover means are coated with an anti-reflection coating such that the overall loss for the S-polarized light is somewhat greater than the overall loss for the P-polarized light at said nominal free-space wavelength, thereby minimizing the [worst case] maximum PDL.
- 16. The enhanced volume phase grating of claim 12 wherein the external surfaces of said transparent medium and said transparent cover means are coated with an anti-reflection coating such that the overall loss for the S-polarized light is somewhat greater than the overall loss for the P-polarized light after two passes through said enhanced volume phase grating at said nominal free-space wavelength, thereby minimizing the [worst case] <u>maximum</u> PDL in a two-pass design.